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A Study of the Dielectric Strength of Air

Electrical Engineering

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A STUDY OF THE DIELECTRIC STRENGTH OF AIR

BY

LEO MAHLON APGAR

B. S. University of Illinois, 1912

THESIS

Submitted in Partial Fulfillment of the Requirements for the

Degree of

MASTER OF SCIENCE

IN ELECTRICAL ENGINEERING

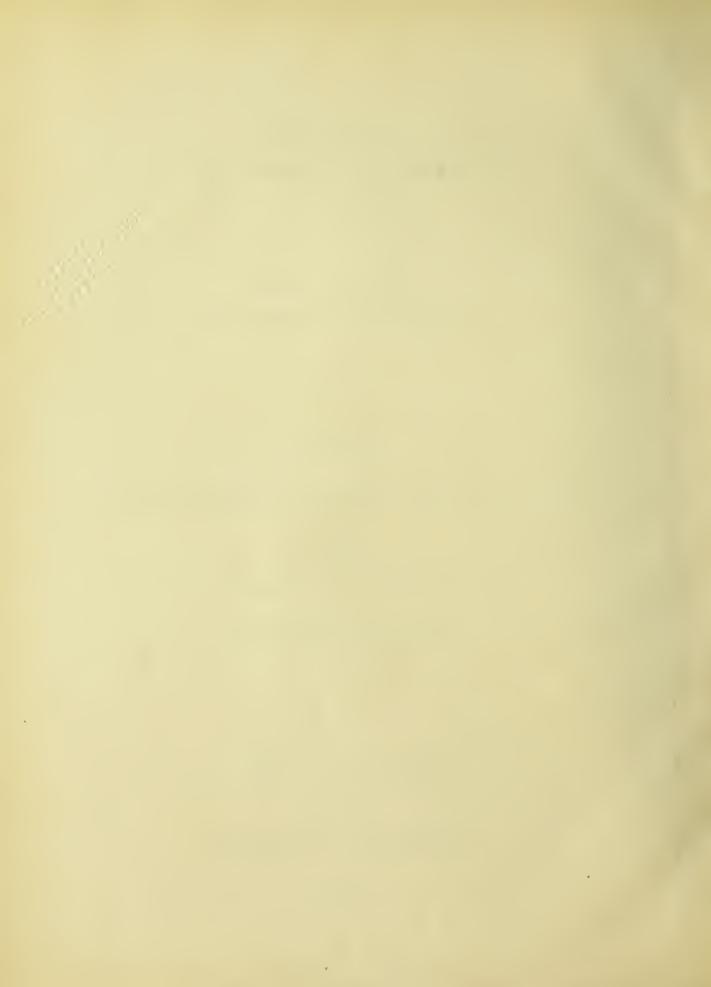
IN

THE GRADUATE SCHOOL

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UNIVERSITY OF ILLINOIS

1913



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May 31 1943

I HEREBY RECOMMEND THAT THE THESIS PREPARED UNDER MY SUPERVISION BY

Leo Mahlon Apgar

ENTITLED A Study of the Dielectric Strength of Air.

BE ACCEPTED AS FULFILLING THIS PART OF THE REQUIREMENTS FOR THE

DEGREE OF Master of Science in Electrical Engineering

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In Charge of Major Work
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Recommendation concurred in: Morgan Brooks. SM. Bugant Ellery Blaine.

Committee

Final Examination



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- III. GENERAL THEORY.
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I. INTRODUCTION.

It is well known that an electric field exists around a charged body placed in a dielectric and it is known that the strength of the field and its distribution depends upon the charge and shape of the charged body. It is believed that if no ions are present, the field might be uniform between the coatings of a condenser consisting of two parallel plates and that its intensity varies inversely as the square of the radius when the charge is given to a sphere isolated in space. It is suspected that the dielectric is only able to sustain a certain intensity of electric field; so that when the field becomes too dense, that is when the potential gradient is too great, the dielectric breaks down. Based upon a number of experiments at which however direct current at rather low voltage was used it was concluded by scientists years ago that the maximum gradient that air could sustain was 30,000 volts per em.

It is the principal purpose of this thesis to determine the maximum value of the potential gradient of air by means of alternating currents at high voltages. The major work was done by subjecting two equal spheres separated by various distances to high potential differences. A small amount of work - largely for checking purposes - was done with needles instead of spheres. The point of breakdown was assumed to correspond to that particular voltage at which corona first appeared.



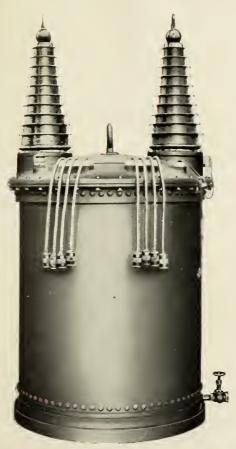


FIGURE 1
A 200,000 VOLT TRANSFORMER
Courtesy The General Electric Co.



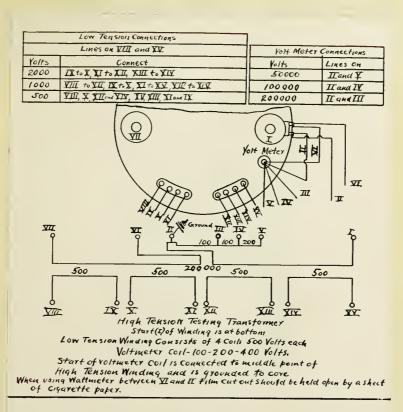
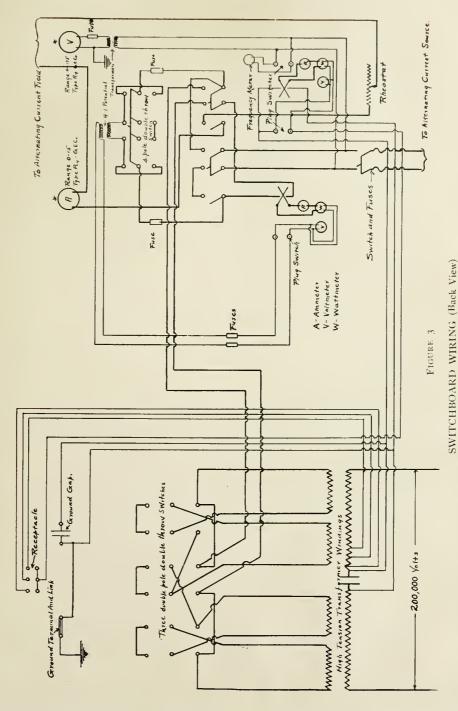


FIGURE 2





SWITCHBOARD WIRING (Back View)
All Meters Not Marked With * Are Enclosed in Drawers



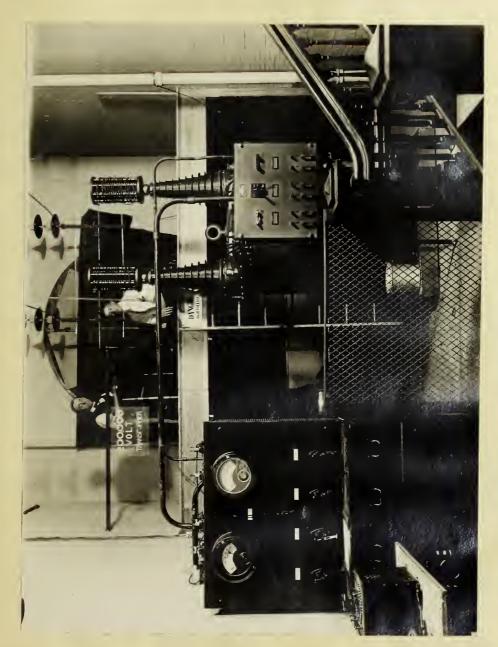


FIGURE 4 General Layout Of Apporatus



The high voltages used were obtained from a special testing transformer (Fig. 1.) manufactured by the General Electric Company which was of the following rating.

Capacity: - 100 W.W. at 60 cycles.

Voltage Ratio: - 500-1000-2000 to 200,000.

Current Ratio: - 50-0.5.

Ratio of windings as used: - 400 to 1.

For all tests the neutral of the transformer was grounded.

As shown in Fig. 4 two switchboards were provided. The one to the right, near the transformer, contains the low tension coil grouping switches and high tension instrument taps which are shown in the left of Fig. 3.

On the switchboard to the left in Fig. 4 are mounted the control switches and meters. All meters in the transformer circuits are in drawers which are covered with plate glass. These drawers are so constructed that all connections are broken when drawers are opened. The circuits on this board are shown on right of Fig. 3.

To limit the flow of current between the spark gap terminals on breakdown of the gap, non-inductive resistance was inserted. As it was desired to limit the current to one tenth amperes at 200,000 volts pressure 2,000,000 ohms of resistance were needed. Carborundum rods were experimented with but these gave varying resistances and had a negative resistance coefficient; therefore two glass tubes, filled with distilled water to which dilute sulphuric acid was added, were used and they could easily be adjusted to 1,000,000 ohms per tube.

To prevent travelling waves in the transformer windings, two choke coils of 40 turns of #14 wire each, wound on spools of dimens-



ion Sincles by 16 inches, were placed in series with the gen.

The sperk gap apper tus (Tig. 5.) was suspended from to heavy copper rods held by strings of four suspension insulators and consisted of two vertical wooden strips clamped to two horizontal lase

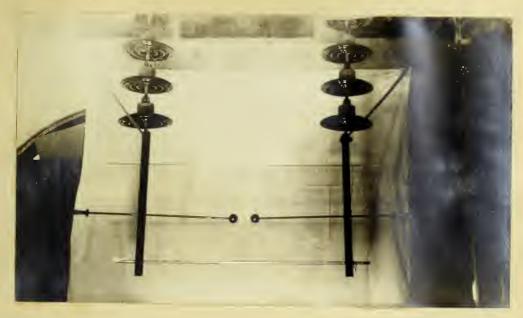


FIGURE 5

brass bearings which were connected to the transformer. In these bearings rested brass rods which had their ends threaded; so that the spheres could be attached. By sliding the rods in or out the various gap lengths could be obtained and measured by means of calipers.

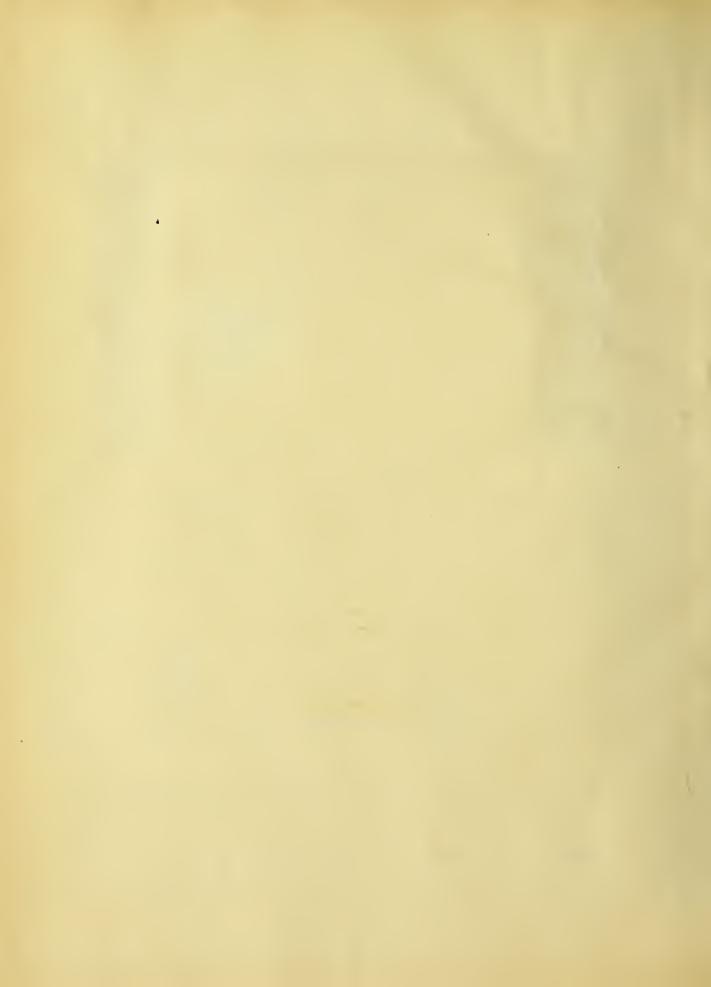
Three different electric generators were used; so that the effect of the wave shape might be studied. The wave shapes are given in Fig. 6.

The rating of above mentioned m chines are as follows:

45 K.W. ESTINGHOUSH SET: - 45 K.W., 2 phase, 440 volt generator belted to 45 K.W. 220 volt D.C. motor.

85 K.W. WESTINGHOUSE SET: - Direct connected phase 440 volt generator and 220 volt D.C. motor.

SMOOTF CORE MACHINE: - Thomson Houston Electric Co., 1100 volts



The potential gradient may be defined as the rate of change of voltage with the distance, or if

f, represents the potential gradient

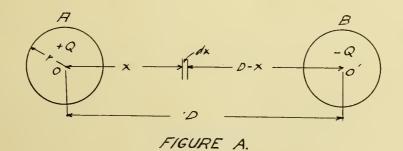
V, the electromotive force or effective e.m.f.

x, the distance between any two terminals.

Then
$$f = -\frac{dV}{dx}$$

To derive a formula for the maximum rotential gradient of air between any two spheres at any distance the theory of electrostatics will be used. To be accurate the system of successive images as given in Maxwell should be used but this would result in a formula too complicated to be of practical use; so the approximate method given below is used and will answer for all practical purposes.

Let A and B in Fig. A represent two equal spheres at any distance charged respectively with a charge + C and -Q. Assume charges to be point charges at O and O' respectively.



The flux $D = 4\pi$

Since $\Phi = 4\pi \Sigma_q$ where q = capacity charges.

Let R be the electric field intensity.

Then
$$R = \overline{0} = \frac{4\pi}{4\pi r^2} = \frac{0}{r^2}$$

At any distance x from a charge Q

$$R = \frac{Q}{X^2}$$



In the following theory, primed letters refer to sphere Λ and double primed ones to B.

Then $R' = \frac{C}{x^2}$ where k' is due to charge on A, and x is distance shown in Fig. A.

$$V = -\int R' dx \quad \text{for air}$$
$$= -\int \frac{Q}{x} dx = \frac{C}{x}$$

$$f' = -\frac{dV}{dx} = \frac{C}{x^2} = R'$$
Similarily $R'' = -\frac{Q}{(D-x)^2} = f''$

And f = f' + f'' (numerically)

Therefore
$$V = Q \left[\frac{1}{x} - \frac{1}{(D-x)^2} \right] = Q \left[\frac{1}{D-x} - \frac{1}{x} - \frac{1}{x} + \frac{1}{D-x} \right]$$

$$= 2Q \left[\frac{1}{(D-x)} - \frac{1}{x} \right]$$

Therefore $Q = \frac{V}{2\left(\frac{1}{D-r} - \frac{1}{r}\right)}$

Substituting value of C in equation for f

$$f = \frac{V}{2\left(\frac{1}{D-r} - \frac{1}{r}\right)} \left[\frac{1}{x} + \frac{1}{(D-x)^2}\right]$$

f is maximum at the surface of the spheres when the corona ball is of the same diameter as the spheres themselves or x = r

Therefore
$$f = \left[\frac{V}{2} \frac{(D-r)^2 - r^2}{r(2r-D)(D-r)} \right]$$

But 2r-D = -X

Therefore $f = -\frac{V}{2X} \left[\frac{(D-r)^2 - r^2}{r(D-r)} \right]$

Since X in this formula is the distance between the fictious corona balls it becomes necessary to find their diameters. Just before corona appears it is evident that the corona ball and sphere



must be of the same diameter since immediately after corona is 10 visible the corona ball is the larger; therefore one is now confronted with the proposition of finding the length of gap at which corona first appears.

As this distance is very difficult to observe, especially if it is not known within two or three centimeters, a graphical method of finding it is developed below.

Up to a certain length of gap between the spheres only break-down occurs. After this point (which will be called the critical point) is reached corona will first appear and then if the voltage is increased breakdown will occur at a higher value, depending upon the length of gap.

It was found experimentally that the corona voltage followed a smooth curve which was somewhat similar to a parabola while the breakdown voltage varied in a straight line for several thousand volts after the critical point had been passed. If the breakdown line (the straight line) is produced to intersect the corona line, the point of intersection will give the distance and voltage at which corona first appears, and this distance and voltage is the one used in calculating the maximum potential gradient.

Geo. R. Dean of the University of Missouri has deduced a formula for the lotential gradient, using point charges. By means of trigonometry he has expressed the gradient as

$$f = \frac{V}{4X} \left[\frac{X}{\rho} + 1 + \left[\left(\frac{X}{\rho} + 1 \right)^2 + 8 \right] \right]$$

where X is length of spark gap,

and ρ is radius of curvature,

V is effective potential difference.

The maximum difference between the values of the gradient computed



11

by this formula and those computed by lussell's is about one-half of one percent and occurs in the neighborhood of $\frac{1}{a}$ = 1.5, X being spark gap and a the radius.

Table #10 shows the potential gradients as calculated by the three different methods and the percent difference between them.



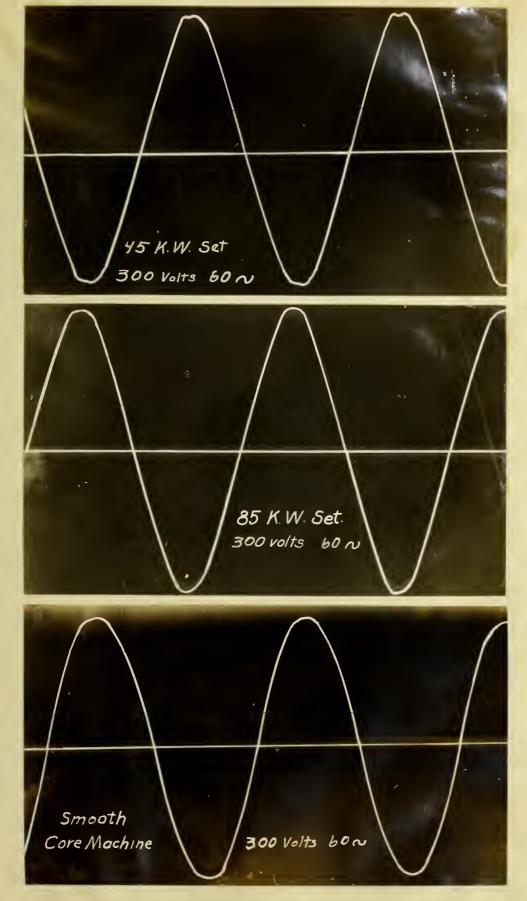


FIGURE 6



IV. DATA AND DISCUSSION OF FESULTS.

Article 1.

Needle Caps.

All the results tabulated are the average of two or more readings for each length of gap (X) during a test.

Along with the study of potential gradient and corons the needle gap was investigated. Sharp's No. 1. needles were used throughout the tests. In Plate I. the points obtained by using the 45 K.W. set were plotted along with Feek's and the A.I.E.E. curves. Feek has straight lines which intersect at 35,000 volts and 5 cm. distance, the A.I.E.E. gives a curved line sterting at zero, while the data obtained in the tests, using the 45 K.I. set, gives a line with a reverse curve in it. Thinking that perhaps the wave shape of this set was such that resonance was obtained which would affect the results, two other machines, an 85 K.W. set and a smooth core generator, were also used and data obtained. This data is given in table #1 and plotted in Plate II.

The wave shapes of each of the machines can be seen by referring to Fig. 6. which gives the oscilliograms taken from each.

Referring to Plate III. it will be seen that the smooth core machine which has practically a sine wave, gives a curve that comes nearer coinciding to that of the A.I.E.E. but even at the best does not follow it closely. The 85 K.V. & 45 K.W. sets have nearly the same wave shape as can be seen by referring to Fig. 6. and the curves for the needle gaps are practically the same, the ordinates of the 85 K.W. one being a trifle higher.

Dr. C. P. Steinmetz states that the breakdown of the air is due to the maximum value of e.m.f. Referring again to Fig. 6. it



will be noted that even though all the effective values of e.m.f. are the same, the meximum value of the smooth core machine is the smallest, and then referring to Plate 2. it will be observed that for the same gap a higher effective e.m.f. is required for breakdown with the smooth core machine which means that the maximum had to be increased to that of the other machines.

In table #2 the results of an investigation of the effect of size and shape of terminals on the breakdown voltage of the needle gap are tabulated. It was found that placing of conducting materials such as balls of tinfoil back of the needle points made no difference in the breakdown voltage but that the length of needle protruding beyond holder increased the voltage necessary for breakdown.



TABLE #1.

FOR NEEDLE POINTS.

Temp. 27 C.

Rel. Humidity 56-53%

				0	
X cm.	BREAKI	DOWN VOLTACES	}	NOTES	
	Smooth Core KV.	85 K.W. KV.	45 K.W. KV.		
4 8 10	30.5 53.5	30.0 51.5	28.0 49.5	Sharps #1 Used	Needles
12 14	71.3	69.0	58.0 66.5 72.5		
16 18	80.5	78.0	77.5	86.0 after	hrankina
20 22	88.5	89.0	89.0 92.0	95.0 after	
24 26	97.5	98.0	99.0	109.0 "	or caking
28	109.0	109.0	108.5	130.0 "	11
32 34	120.0	112.0	119.5		
36 38 40	131.0	124.0	128.0		
42 44	140.5	135.0	139.0		
46 48	152.0 164.0	146.0	152.0		
50	104.•0	161.0	165.0		

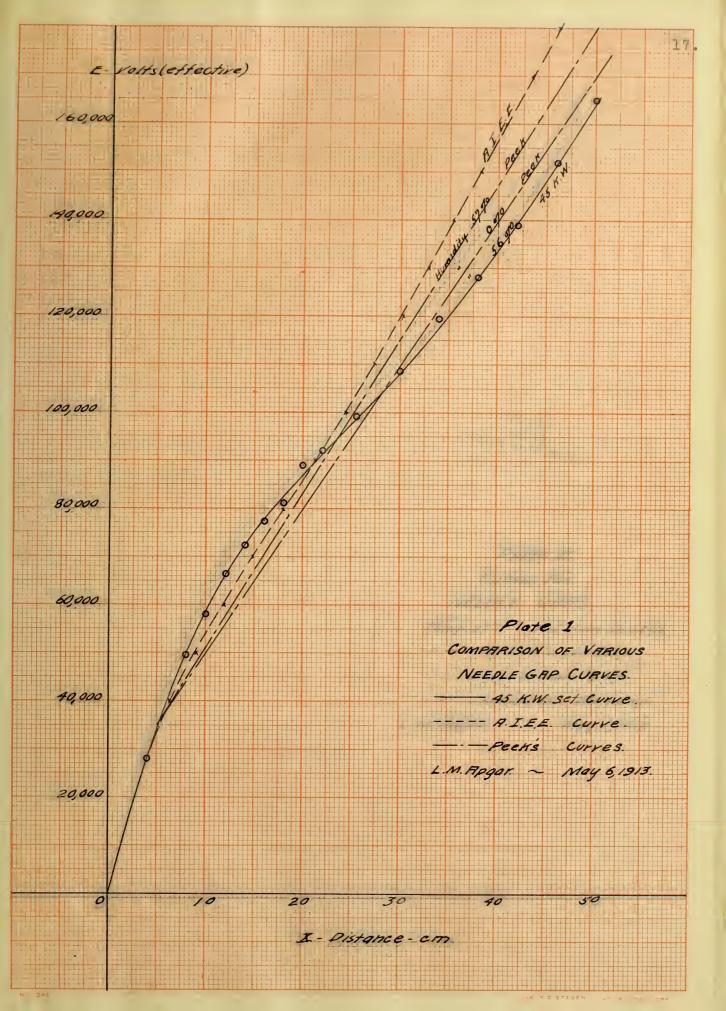


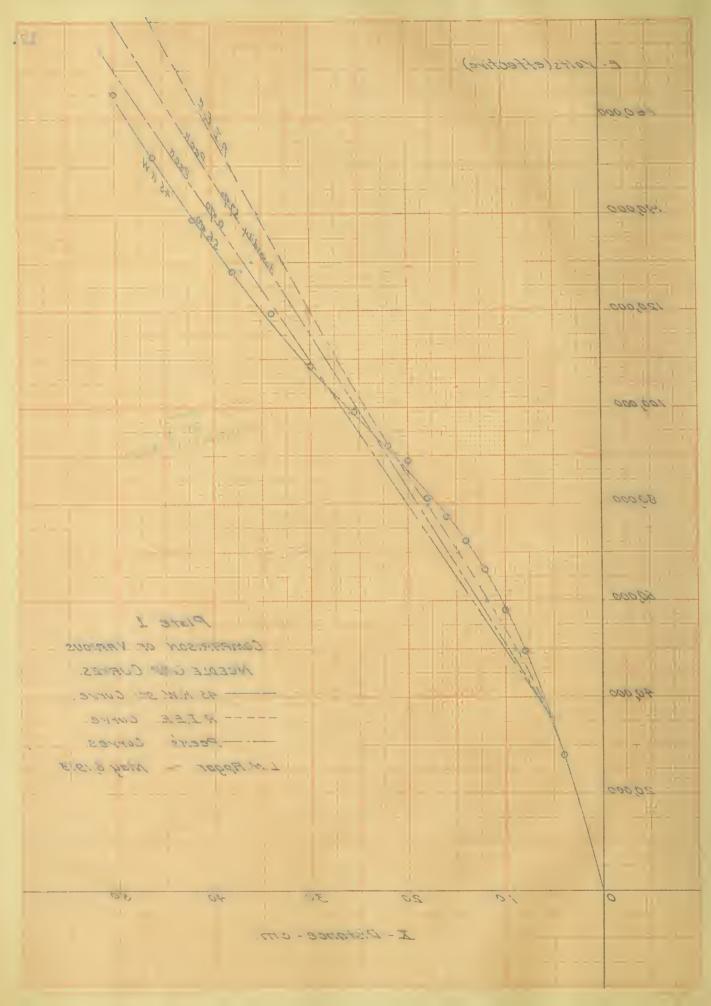
TABLE #2

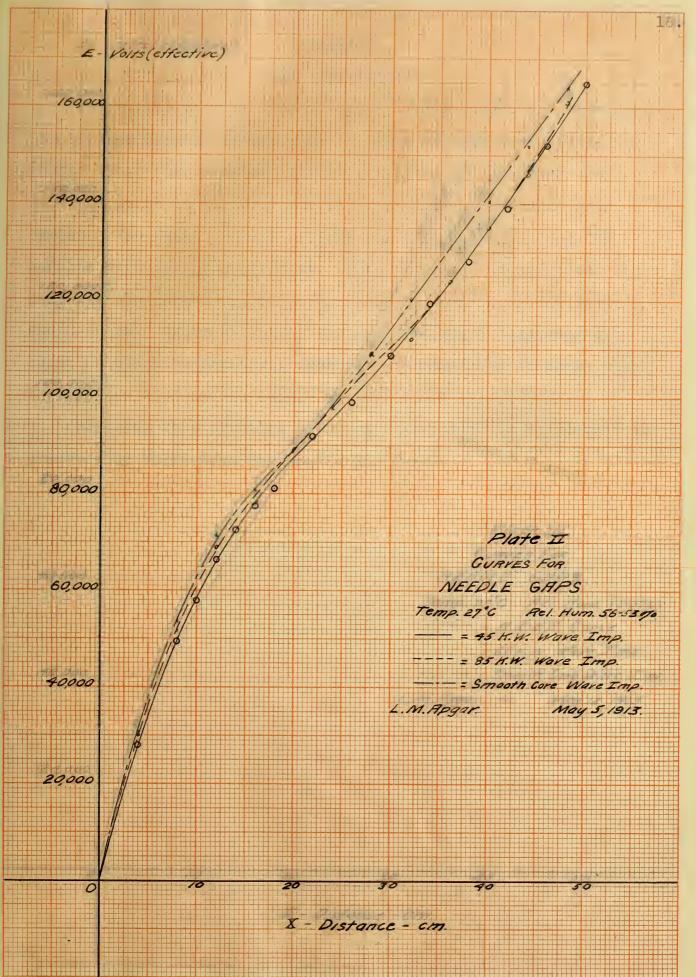
EFFECT OF TERMINALS ON NEEDLE GAP.

Tem	p. 27 C	Relative Humidity 56-53 %
X	Breakdown	Notes.
em.	EV.	
10	58	3 cm. of needle protruding.
	56	1 cm. " " "
	59	blast of air on 3 cm. of needle.
	58	point just beyond tinfoil ball.
50	165	3 cm. needle protruding.
	1 65	4 cm. "
	164	1 cm. "
	165	blast of air on 3 cm.
	165	tin foil around rod.
	170	point just beyond tinfoil ball.
	165	2 ft. disks on rods.

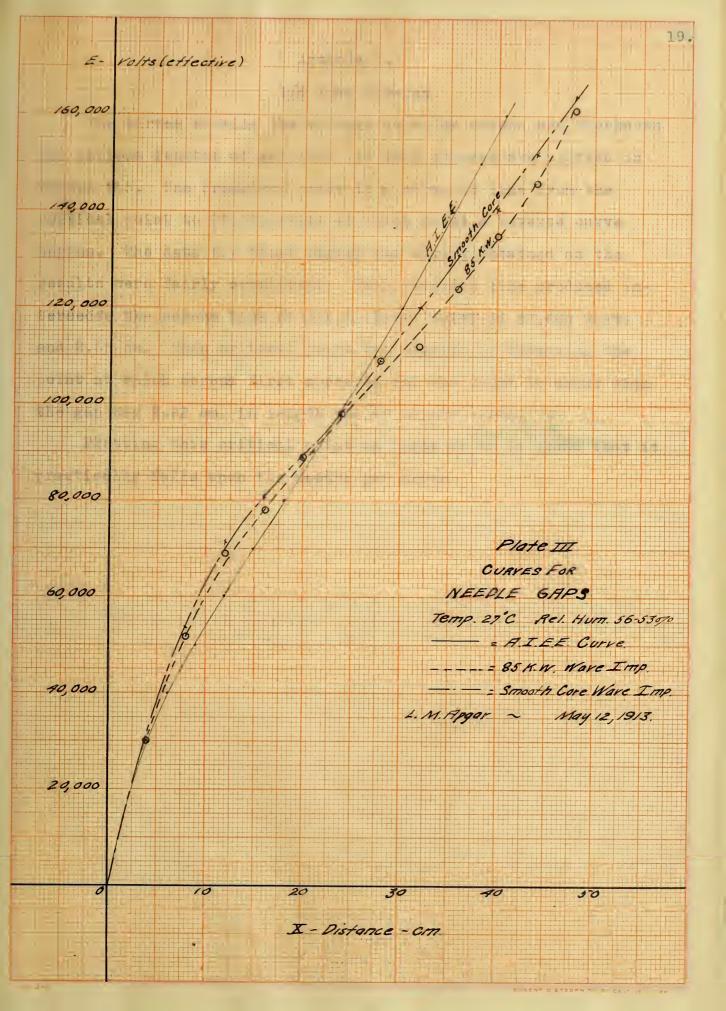


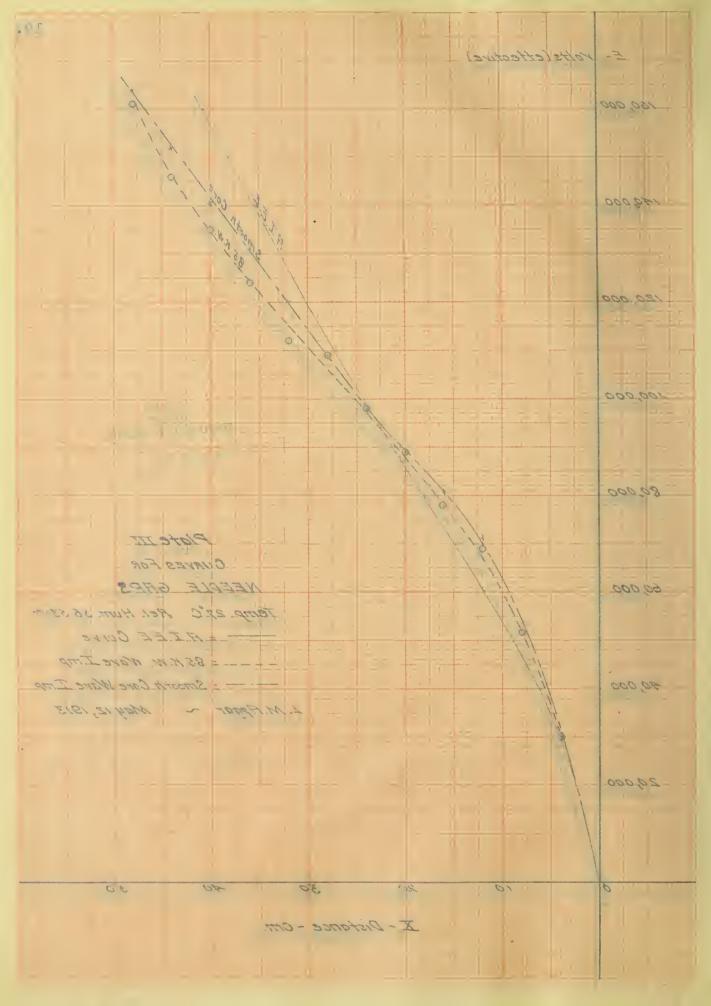






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Article 2.

1/4 Inch Spheres.

The curves showing the voltage at which corona and breakdown for various lengths of gap with 1/4 inch spheres are plotted in Plates 485. The breakdown curve is a straight line from the critical point to 98,000 volts at which point a reverse curve begins. The data for these curves was easily obtained as the results were fairly consistent. This straight line produced intersects the corona line at the critical point of 22,600 volts and 2.65 cm. This critical point was checked by observing the point at which corona first appeared and was found to occur when the gap was 2.65 cm. in length and at 22,600 volts.

Plotting this critical point on Plate XI it is found that it practically falls upon the needle gap curve.

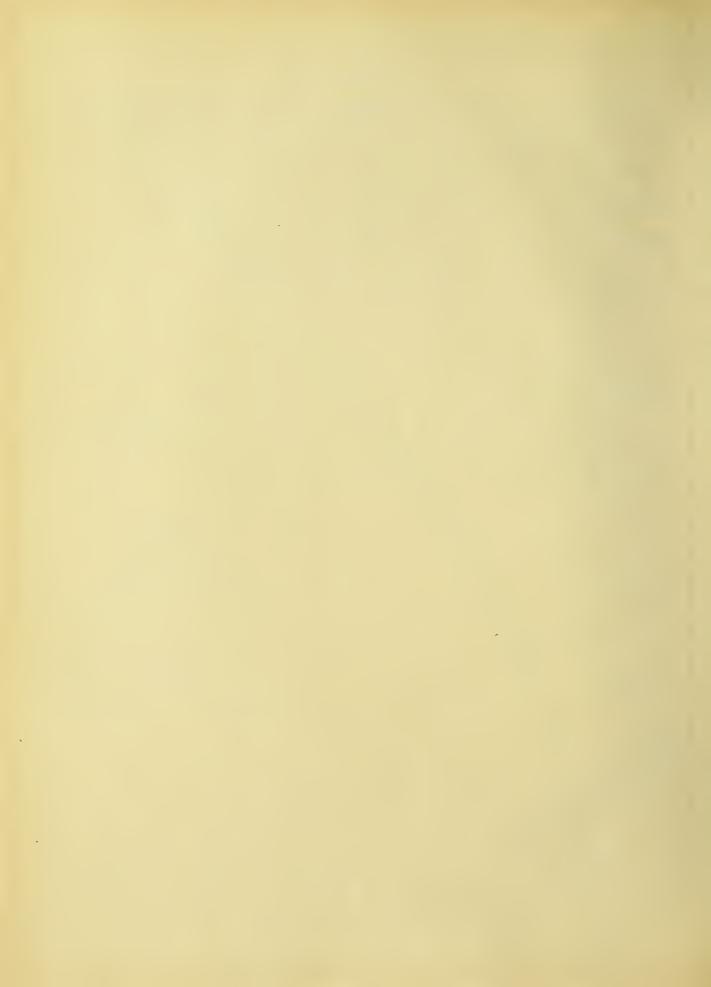
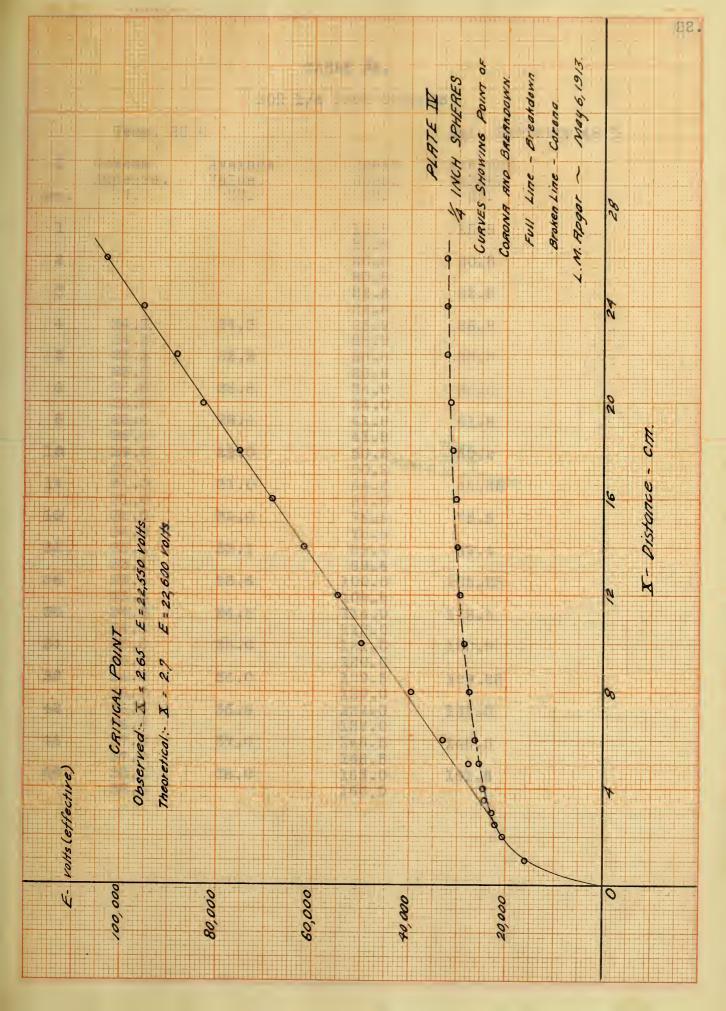


TABLE #3.

			TABLE #3.		
	Temp. 26	01. 1/	4 INCH SPHERE		dity - 50 %
X	Corona		7) 3		
	Appears	Average Value	Br ea k down	Average Value	Notes
cm.	KV.	KV.	KA.	MA.	
1.0 2.0 2.5 3.0 3.5 4.0	24.6	24.6	25 . 2	16.0 20.6 22.2 23.2 24.2 25.2	
5 0	24.6		25.2		
5.0	00.0	25.4 26.4 27.6		27.8 33.0 3 9. 8	
10.0	29.0 28.6	28.9	50.0 50.0	50.0	polished not polished
12.0	29.4 29.4	29.4	55.0 55.0	55.0	polished not polished
14.0	30.0 30.0	30.0	62.0 62.0	59.0 62.0	with fan
16.0	30.5 30.0	30.25	69.5 68.0	68.75	
18.0		31.0	76.5 74.0	75.25	
20.0	31.5 31.5	31.5	83.0 83.0	83.0	polished not polished
22.0	32.5 72.5	32.5	89.0 88.0 88.0	86.5 88.3	with fan
24.0		32.5	96.0 95.0	95.5	
25.0	32.5 32.5 32.7	32.56	103.0	103.0	

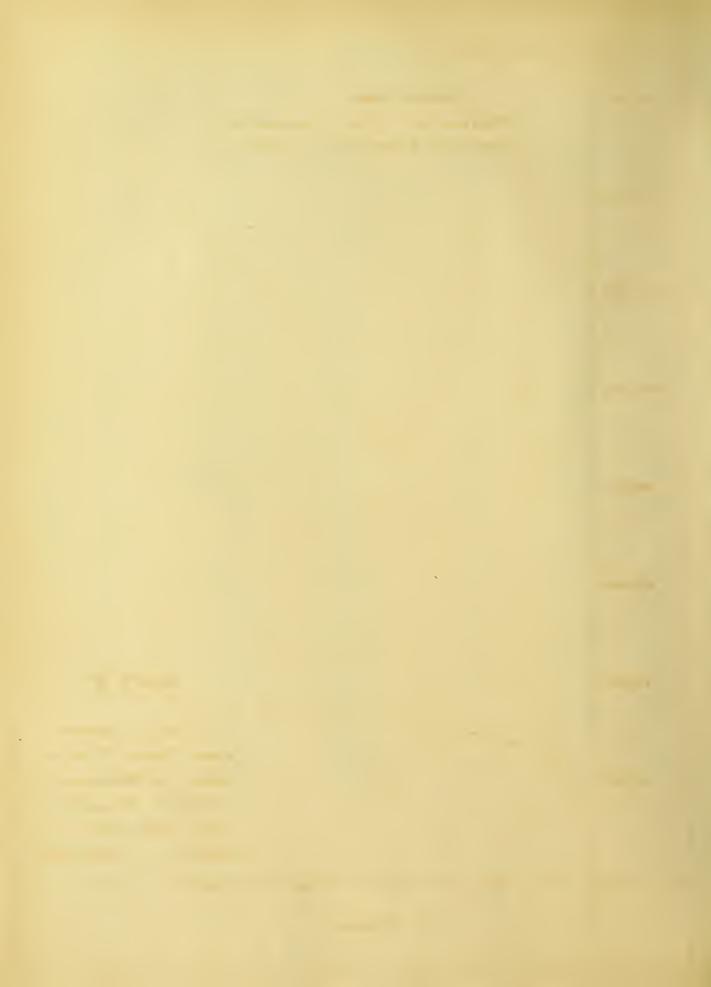


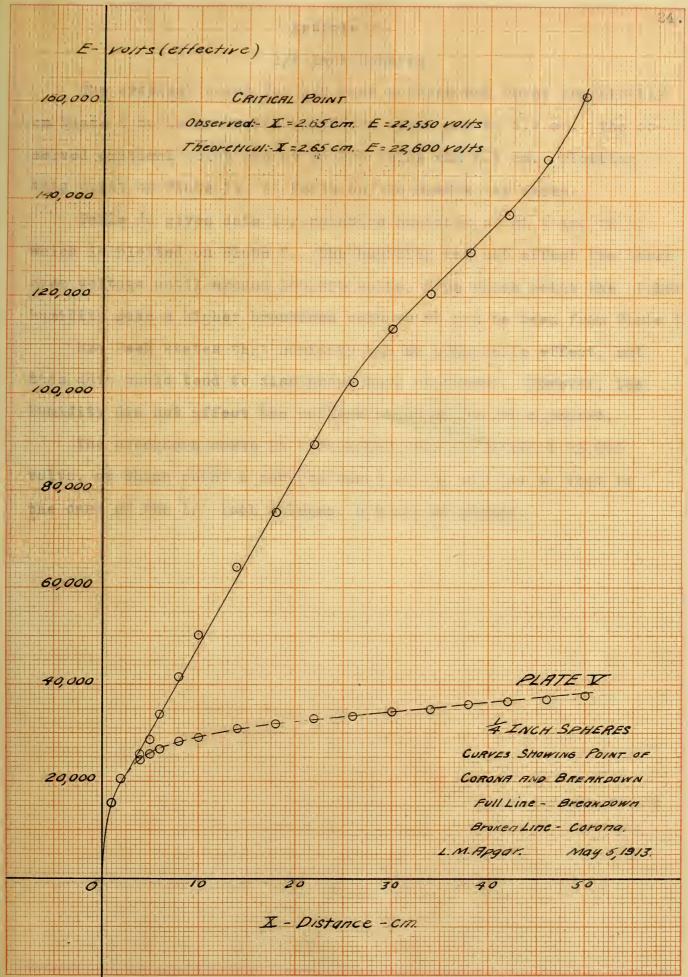


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TABLE #4.
FOR 1/4 INCH SPHERES.

	Temp. 23	3 C		Rel. Humidity 48 %
X	Corona	Average	Break	Average
	Appears.	Value.	down.	Value.
em.	··V.	··V.	KV.	KV.
1			15.8	15.8
			15.8	
2			20.8	20.8
_			20.8	
3			22.8	22.8
4	24.3	94 7	22.8	
4	24.3	24.3	25.9 25.9	25.9
5	25.5	25.5	28.8	28.8
	25.5	~0•0	28.8	20.0
6	26.8	26.8	34.0	34.0
	26.8		34.0	
8	28.4	28.4	41.8	41.8
	28.4		41.8	
10	29.0	29.0	50.2	50.2
7.4	29.0	57.0	50.2	
14	31.0	31.0	64.5	64.25
18	31.0 32.0	70.0	64.0	w.r
10	32.0	32.0	75.5	75.5
22	33.1	33.1	75.5 89.4	89.4
~~	33.1	00 • T	89.4	05.4
26	33.6	33.6	102.0	102.25
	33.6		102.5	
30	34.5	34.5	114.0	113.5
	34.5		113.0	
34	35.0	35.0	121.0	120.5
70	35.0	7.4	120.0	
38	36.0	36.0	129.5	129.25
42	36.0 36.5	76 F	129.0	7.78
TA	36.5	36.5	137.0 137.0	137.0
46	37.0	37.0	148.5	148.5
	37.0	01.0	148.5	T-20.0
50	38.0	38.0	163.0	161.5
	38.0		160,0	





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1/8 Inch Spheres.

The critical point for 1/2 inch s heres was found grathically on Plate 6 to be at 39,500 volts for spark gap of 5.7 cm. The observed critical point was at 40.000 volts and 5.7 cm. Plotting this point on Plate 11, it falls on the needle sap curve.

Table #6 gives data for relative humidity of 56 and 40, which is plotted on Plate 7. The humidity did not affect the spark over voltage until around 100,000 volts, from which point the ligher humidity gave a higher breakdown voltage as can be seen from Plate 7.

Mr. Peek states that humidity has no measurable effect, but this data would tend to disa prove that statement. However, the humidity did not affect the voltage at which corona appeared.

The breakdown curve is a straight line up to about 82,000 volts, at which point a reverse curve starts similar to that in the case of the 1/4 inch spheres, but not so marked.



TABLE #5.

FOR 1/2 INCH SPHERES.

	Temp.	26 C.		Rel. Humidity - 50
X	orona	Average	Break-	Average
cm.	Appears KV.	Value KV.	down KV.	Value KV.
2			28.4 28.4	28.4
3			32.8	32.9
4			33.0 36.0	35.75
5			35.5	70 7
Ð			38.2 38.0	38.1
6			40.0	40.0
7			40.0 41.0	41.2
8			41.4 42.0	42.15
			42.3	±
9			43.5	43.2
10	44.0	44.2	51.0	51.0
11	44.4 44.5	45.0	51.0	EA ME
7.1	45.5	40.0	54.5 55.0	54.75
12	45.0	45.5	56.5	56.25
	46.0		56.0	
13	46.2		59.5	59.5
			59.5	
14	46.8		63.0	62.5
	4 77 0		62.0	
15	47.0		66.5	66.25
16	47.5	47.4	66.0	60.0
10	47.3	± f • ±	68.0 68.0	68.0
17	48.0		72.0	
18	48.5		74.5	
19	49.0		76.5	
20	50.0	49.75	80.5	80.75
	49.5		81.0	
22	51.0		88.0	
24	51.9		92.5	92.5
			92.5	
26	52.5		98.0	98.0
			98.0	



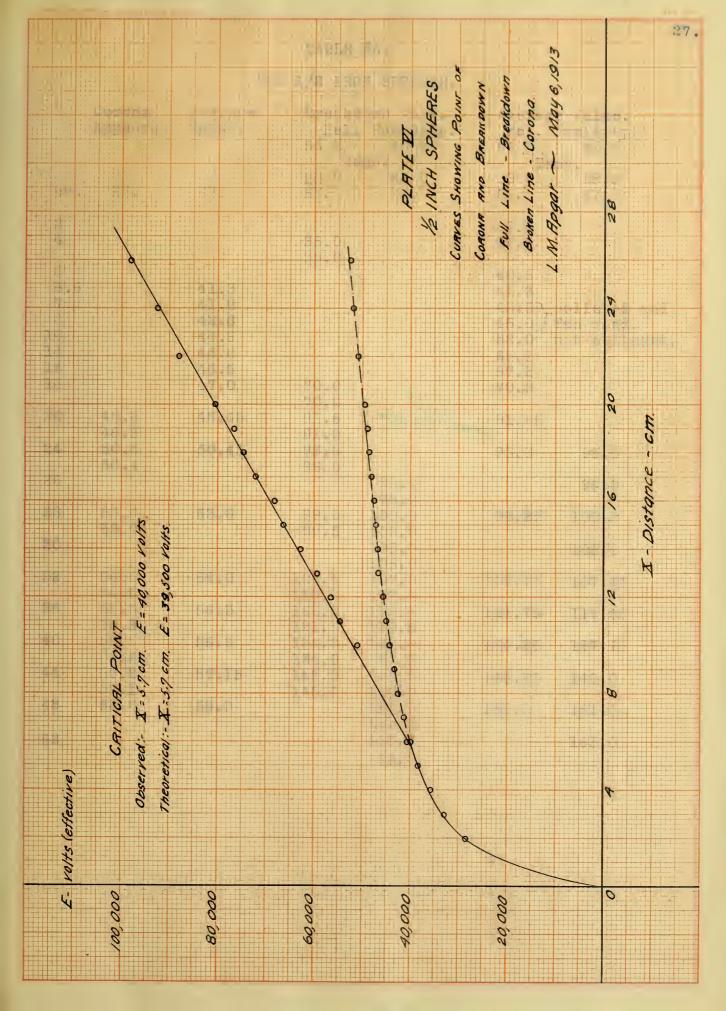
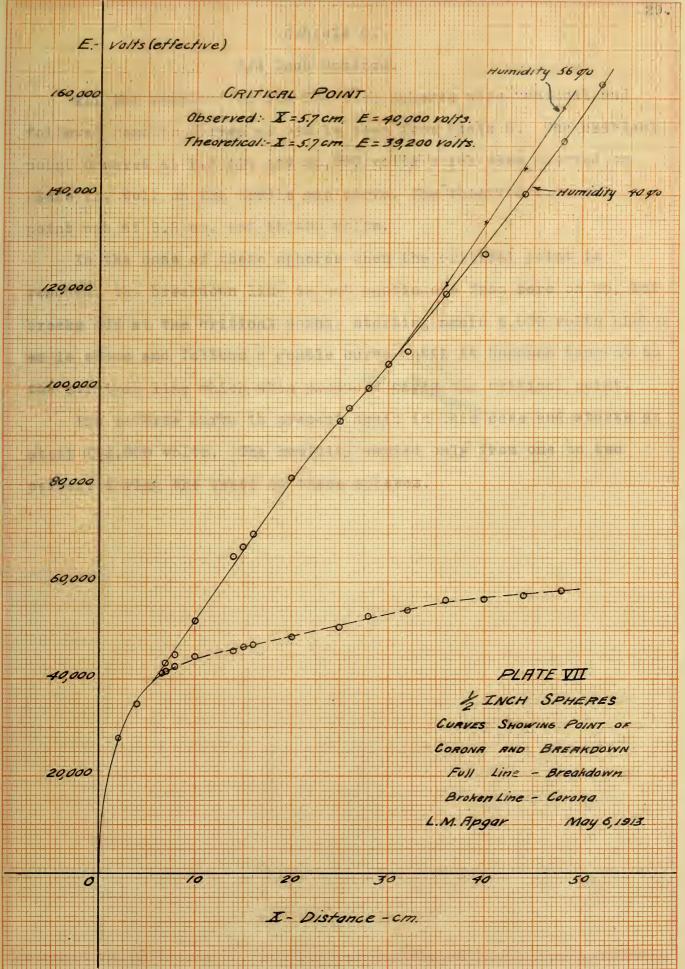


TABLE #6.

FOR 1/2 INCH SPHERES.

	Corona Appears.		Rel 56 %	down Volt Jumidity. 40 d	56 %	e Value. Humidity. 40 ¶ mp. 23 C
cm.	KV.	· . V •	KV.	ZV.	MV.	KV.
2 4			35.0 35.0		28.0 35.0	
6 6.6 7 8 10 14 15 16		41.3 41.8 42.8 44.8 45.8 46.5 47.0	70.0 70.0		45.0	polished and fan used.
20	48.8	48.65	81.5		81.25	
24 26	48.5 50.5 50.4	50.45	81.0 93.0 93.0		93.0	93.0
28	53.0	53.0	99.0	96.0 96.0 100.0	99.25	96.0
30	53.0		99.5	100.0		105.0
32	54.0 54.0	54.0	109.5	105.0	109.75	107.25
36	56.3 56.3	56.3	110.0	107.5	121.75	119.55
40	56.5 56.5	56.5	121.5	119.5	134.25	127.75
44	57.2 57.1	57.15	134.5	127.5 140.0	145.25	140.0
48	58.0	58.0	145.5	140.0	158.0	151.0
52				151.0 163.0 163.0		163.0





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Second Deserved: 2 45 per E 2 40 per 101. Therefored: 2 47 per E 2 49 per Velts. Therefored: 2 47 per E 2 49 per Velts. Therefored: 2 47 per E 2 49 per Velts. Therefored: 2 40 per E 2 49 per Velts. Therefored: 2 40 per E 2 40	E. Volts letteshive)	
Second Conserved: 2 55 pm 6 2 50 pm	Humidity 36 go /	
Aces of the state		
Theraphort I Som E Specie rain. According to a second sec		Ta)
ACOCO SECOS SE		
ACOCO SECOS SE	Theoretical:-I=5.7cm. E=39200 volts.	<u> </u>
Secon		
Secon		
Second Se	000 05 A A 10 20 A A A A A A A A A A A A A A A A A A	
Second Se		+
Second Se		
Second Se		
Second Se		7.7
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Sacoo Sa		
Decool Second Second	20208	
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ACOCO PO SONO AL TIMEN SINGERES SOCIO FUN LINE - SINGH ONN STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED		
ACOCO PO SONO AL TIMEN SINGERES SOCIO FUN LINE - SINGH ONN STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED LINE - CAP NO LINE - STORED LINE - CAP NO STORED		
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AGGOO SONERS SHOWING FUNT OF SONE FUND OF SONE FUNT OF SONE FUND OF SONE FU		
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Sucurine Paint o Canavin sind Bire Kodinin Suchem Line - Breakdown L., Hogar May 6, 15 Z-Lis, whee - cm	t then Someres	
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Article 4.

3/4 Inch Spheres.

All the results for the 3/4 inch spheres were rational and followed regular curves as can be seen from Plate 8. The critical point occured at 9.3 cm. and 55,000 volts which when plotted on Plate 11. fell on the needle gap curve. The observed critical point was at 9.2 cm. and 55,400 volts.

In the case of these spheres when the critical point is reached, the breakdown line is not continuous from zero on up, but breaks off at the critical point, starting again 4,000 volts higher as is shown and follows a gentle curve until it becomes tangent to the streight line which when produced gives the critical point.

The reverse curve is present again in this case and starts at about 102,000 volts. The humidity varied only from one to two percent during the tests on these spheres.



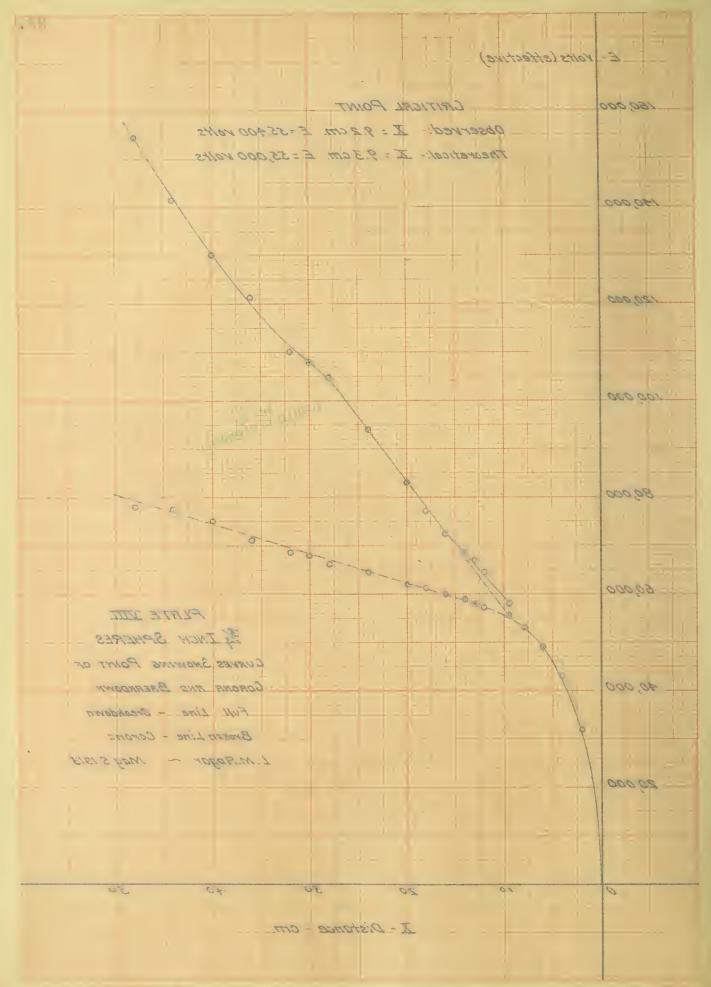
TABLE #7.

FOR 3/4 INCH SPHELES.

	Temp. 22	С.	Rel	ative Humi	dity - 48 %
X cm.	Corona Appears.	Average Value. KV.	Break- down. WV.	Average Value. V.	Notes
2 4 6 8 9				32.0 43.2 49.0 53.0 54.0 55.4	
9.25 9.3 9.5	56.2	55.5 55.6 55.9		56.6 57.6 58.0	
11 12	56.5 57.2 57.2	57.2	65.0 64.0 57.0 57.0	64.5	lished,& fan used but no corona.
12.5	57.5	57.5	64.0	64.9	bat no colona.
13	57.5 58.0 58.0	58.0	65.8 67.5 66.5 67.0		t polished. eshed before cor.
14	59.0	59.0	68.7	68.65 No	flash
16	5 9.0 60.0	60.0	68.6 72.5	72.5	St. Williams
18	60.0 61.2 61.2	61.2	72.5 7 7. 0 77.0	77.0	Talenta de Caración de Caració
20	62.0 62.0	62.0	83.0 83.0	83.0	interpretation of the control of the
24	64.5 64.5	64.5	94.5 94.5	94.5	And the second s
28	66.2	66.25	105.0	105.0	aberic provinces
30	68.0 68.0	68.0	1.08.0	108.5 Wi 108.0	th fan
32	68.9 68.9	68.9	110.0	110.0	
36	71.0 71.0	71.0	110.0 121.0 121.5	121.25	
40	11.0	75.0	130.0	130.0	
44		77.5	141.0	141.5	
48		78.0	142.0 154.0 156.0 154.0	154.6	



E- Val	its (effective)	
160,000	CRITICAL POINT	
	Observed: I = 9.2 cm. E	= 55,400 volts
-1	Theoretical: X = 9.3 cm. E	= 55,000 volts
150,000		<u> </u>
		, p
120,000		
100,000		
80,000	6	2_2-0-
		-0
	9,96	
60,000	9	
	9/000	PLATE VIII
		1/4 INCH SPHERES
	T. T	CURVES SHOWING POINT OF
40,000	7	CORONA AND BREAKDOWN
		Full Line - Breakdown
		Broken Line - Corona.
20,000		L. M. Apgar ~ May 6,1913.
20,000		
	70 20 30	40 50
	I - Distance -	cm.
	(



Article 5.

1 Inch S heres.

The theoretical critical point of the one inch spheres occurs at 14.4 cm. at 71,000 volts which when plotted on Plate II falls a little below the needle gap curve. The observed value of this point was found to be 14.4 cm. at 71,450 volts.

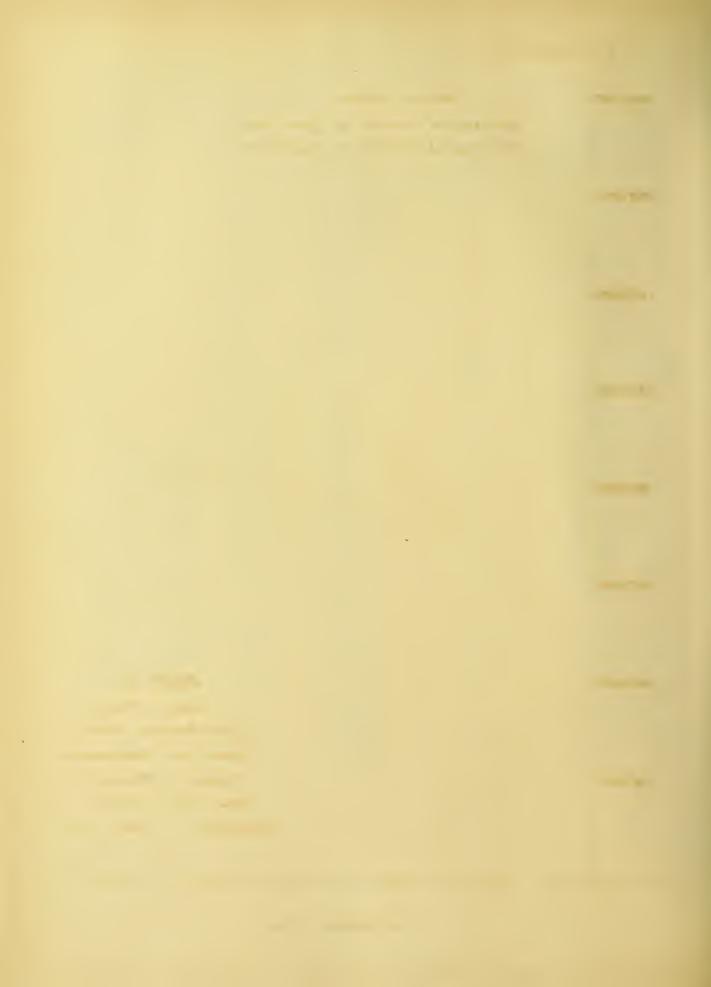
The breakdown line breaks off scain at the critical point and starts 6,000 volts higher, following the same general shape as in the case of the 3/4 inch spheres with the exception that the reverse curve is not present in this case but at 130,000 volts the breakdown line begins to curve gently upward.



TABLE #8.

FOR 1 INCH SPHERES.

	Temp.26	C	Relat	tive Hum	idity - 56 =
X cm.	Corona Appears. KV.	Average Value. KV.	Break- down. KV.	Averag Value kV.	
2 4			34.0 48.5 49.0	34.0 48.75	
6			55.7 55.7	55.7	
8			61.5 61.0	61.25	
10			64.0 64.0	64.0	
12			66.5 67.5	67.0	
14.5	71.5	71.5 71.55	78.0	77.8	
16	71.6 71.6 71.6	71.6	77.8 79.5 79.5	79.5	
20	74.5 74.5	74.5	86.0 86.0	86.0	polished
24	77.0 77.0	77.0	95.0 95.0	95.0	not polished polished not polished
26	77.5 77.5	77.5	100.0	101.0	polished not polished
28	80.5 80.5	80.5	108.5 -108.0	108.25	polished not polished
30	81.5 81.6	81.5	112.0 110.0 109.0	110.3	polished not polished
34	8 2.0 82.0	82.0	121.0	121.25	polished
38	83.0 83.0	83.0	132.0	132.0	not polished polished not polished
42	84.0 84.0	84.0	146.0 145.0 145.0	145.3	no portaned
44	84.2 84.2	84.2	151.0 150.0	150.5	



		35.
£-	Volts (effective)	
160,000	Observed:-I = 14.4 cm. E = 71.450 volvs.	
	Observed:-I = 14.4 cm. E = 71,450 rolls. Theoretical:-I = 14.4 cm. E = 71,000 volts.	
140,000		
120,000		
100,000		
80,000		
60,000		
40,000	PLATE IX	
	CUTVES ShowING POINT OF	
	CORONA AND BREAKDOWN	
20,000	Full Line - Breakdown Broken Line - Corona	
	L.M. Apgar. May 5, 1913	
0	70 20 30 40 50	
	X-Distance - Cm.	

	-
s(effective)	E - Volt.
CRITICAL FOINT	
Observed:+Z = 144cm. E = 7/450 volts.	Hi Hira
Theoretical: I = 14.5 cm. E = 71,000 voks.	7
	150,000
	129,000
	1000001
	00008
	60,000
TIBLE IX	\$9,000
LINCH SPINERES COPIES STREETS	v.
CAPARS SIGNAMA CAPARS SIGNAMA	
Full Line - Breakstown	20,000
Branco, Line Coroma LALAPAGO May 2133	
35 6 6	0
I DISTANCE - CM	
	26

Article "6.

2 Inch S heres.

The greatest difficulty was met when experimenting with the two inch spheres. Consistent results were obtained until the neighborhood of the critical point was reached. For spark gaps of 18 to 28 cm. corona would appear at one time and the next the air would break down, sometimes at a lower voltage than that at which corona appeared. The spheres were polished, the fan used between trials, the voltage applied both slowly and quickly, but of no avail. However on applying voltage quickly corona was obtained more often than otherwise. After the 28 cm. gap had been reached no further trouble was experienced with the corona, but the breakdown voltage varied considerable throughout the tests.

The discontinuity in the breakdown line occurs again at the critical point, the rise being 7,000 volts. The reverse curve shows up slightly, starting at about 164,000 volts, but is not very marked

The theoretical and observed critical points check very well both occuring at 20 cm. and with voltages of 116,300 and 116,200 respectively. Plotting this point on Plate 11, it falls about 30,000 volts above the needle gap voltage for 20 cm. This is rather peculiar since in the case of all the other scheres the critical points coincided with the needle gap curve. The reason for this discrepancy is not known.



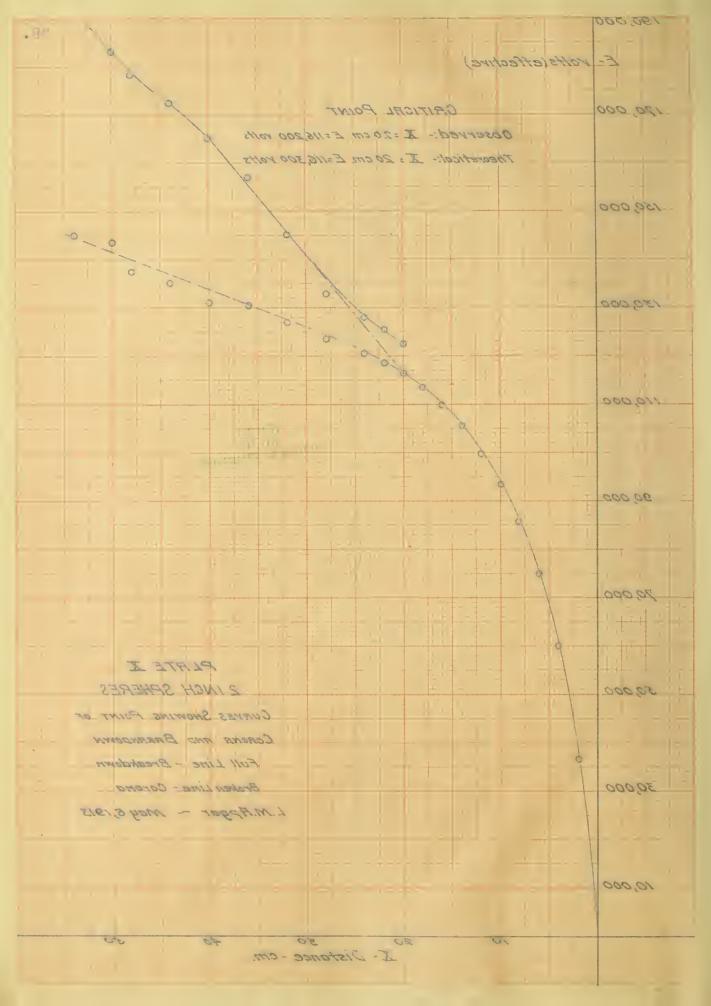
TABLE #9.

FOR 2 INCH SPHERES.

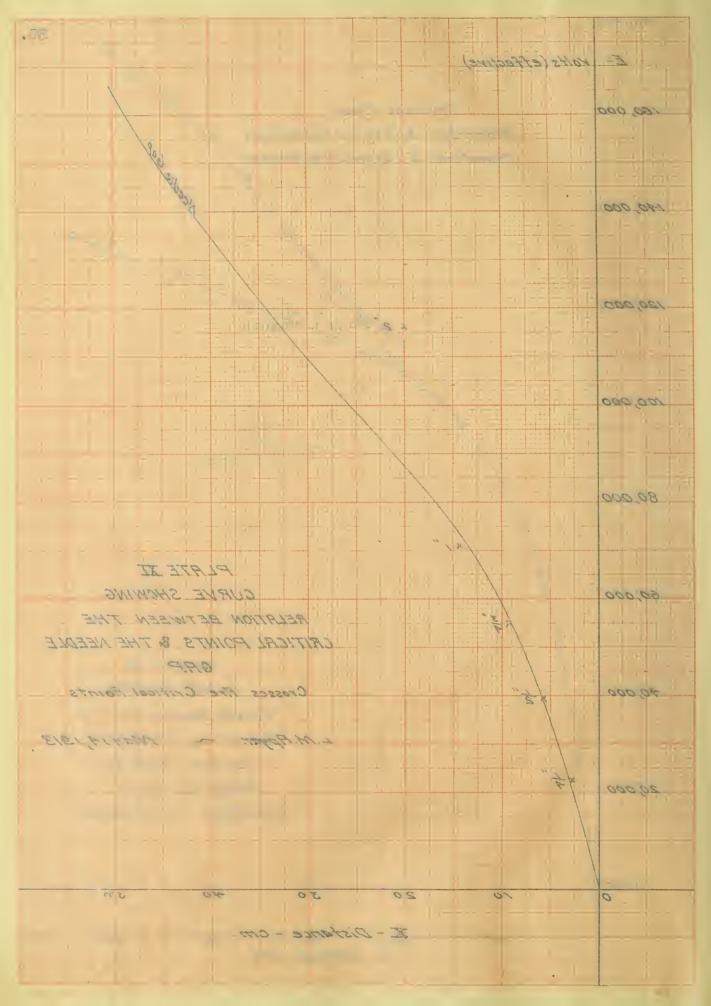
	Temp. 25	C.	k el at	tive Humi	dity - 49 1
X em.	Corona Appears. KV.	Average Value. KV.	Break- down. KV.	Averag Value. KV.	e Notes
	T7 A •	77 A •	17. A •	T7 A •	
2			36.6 36.6	36.6	
4			60.0 60.0	60.0	
6			75.0 75.0	75.0	
8			85.9 86.0	85.95	
10			93.2 93.5	93.35	
12			99.2 100.5	99.85	
14			105.8	105.8	
16			110.0	110.0	
18			113.5 113.5	113.5	
20	116.5	116.5	123.2 122.0	122.6	
22	119.0	118.75	124.0 126.5	125.25	polished
24	120.0	120.5	128.0 128.0	128.0	polished
28	124.0 123.0	123.5	133.0 132.5	132.75	not polished
32	127.0 127.0	127.0		145.0	
36	130.0 130.5	130.25	157.0 157.0	157.0	
40	131.0 131.0	131.0	165.0 165.0	165.0	
44	135.0 135.0	135.0	174.0 171.0 172.0	172.5	
48		137.5	181.0	178.0	
50		143.5	183.0	183.0	
54	145.5 145.5	145.5	193.0 193.0	193.0	
56	147.0 147.0	147.0	198.0	199.0	



190,000			7 38
E- volts (effective			ø
		6	
170,000	CRITICAL POINT		
	ved: X = 20 cm E = 116,200	volts	
Theore	ticol:- X = 20 cm. E=116,300	rolts	
		9	
150,000			
	, , , , , , , , , , , , , , , , , , ,		0 0
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130,000	No.	6 0	
	0/0-0		
	60		
110,000	8		
	ø .		
90,000			
<i>P</i>			
70,000			
ó			
		PLATE X	
50,000		2 INCH SPHER	ES
		CURVES SHOWING POI	2
		CORONA AND BREAKDE	
		Full Line - Breakd	
30,000		Broken Line - Corona L.M.Apgar - May 6	
		will gar - way e	
10,000			
	20 50	40	ro
	X - Distance -		
NO 346		EUDENE C ETZGEN	SH AUTHEN ORP



									39.
									7
E-	volts (e)	fective)					119		
							iiii		
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80,000									
80,000									
80,000		/							
80,000		/x	/ /						
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		/x	,"				TE XI		
60,000		/x	,"				TE XI SHOWIN	6	
			,"		REI	CURVE	SHOWIN		
		/x	/			CURVE	SHOWIN	THE	
			/			CURVE	SHOWIN	THE	(E
			,"			CURVE TION BET AL POINTS	SHOWING WEEN THE	THE	<i>LE</i>
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		k 3 -	,"		CRITICI	CURVE TION BET AL POINTS	SHOWIN WEEN I & THE	THE NEED	(E
50,000		k 3 -			CRITICI	GURVE ATION BET AL POINTS GR	SHOWIN WEEN I & THE	THE NEED	LE.
50,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
50,000		k 3 -			CRITICI	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED	
40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
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40,000		k 3 -			Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 8 THE P Critical F	THE NEED, Points	
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40,000		k 3 -	20		Cros.	GURVE ATION BET AL POINTS GA ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	
40,000		\$ " " " " " " " " " " " " " " " " " " "	20		CRITICI Cros. L.M.A.	GURVE HTION BET HL POINTS GH Ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	
40,000		\$ " " " " " " " " " " " " " " " " " " "	20		CRITICI Cros.	GURVE HTION BET HL POINTS GH Ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	
40,000		\$ " " " " " " " " " " " " " " " " " " "	20		CRITICI Cros. L.M.A.	GURVE HTION BET HL POINTS GH Ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	
40,000		\$ " " " " " " " " " " " " " " " " " " "	20		CRITICI Cros. L.M.A.	GURVE HTION BET HL POINTS GH Ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	
40,000		\$ " " " " " " " " " " " " " " " " " " "	20		CRITICI Cros. L.M.A.	GURVE HTION BET HL POINTS GH Ses Are C	SHOWIN WEEN 7 8 THE Pritical F	THE NEED, Points	



Potential Gradient.

In table #10 the potential, for the critical point of each sphere are tabulated having been calculated by use of the formula developed in the theory and also by Dean's and Russell's formulae. The maximum percent of difference between these values is 1.2 and occurs in the case of the 1/4 inch spheres. A curve showing the relation of the maximum potential gradient to the diameter of the spheres is given in Plate 12. This curve shows that the potential gradient is not a constant but varies with the size of sphere; the smaller the sphere the higher the potential gradient.

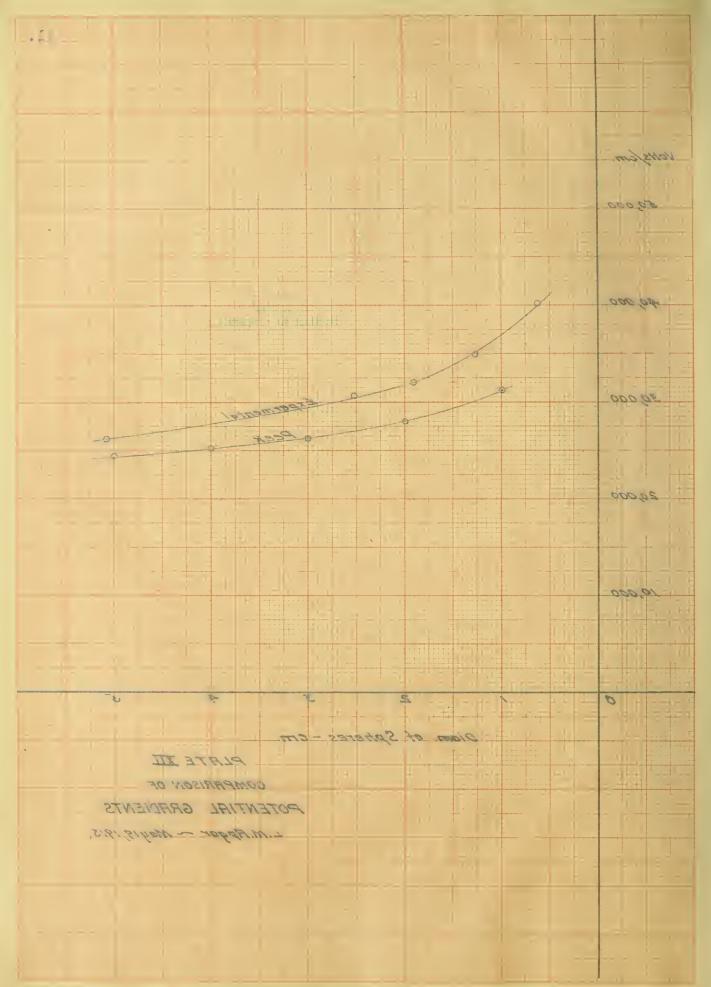
Peek gives a curve that has a similar shape but the ordinates are lower. Take for example a sphere, 4 cm. in diameter; Peek's curve gives about 25,200 volts per cm. for the gradient while the experimental curve gives 27,800 volts per cm.

TABLE #10.

POTENTIAL GRADIENTS. in volts/cm. Dean's Diff. Russell's Diam. of Obser. Theor. Obser. Theor. Sphere. Obser. Theor. Ob. Th. in. em. 5.08 23,100 26,120 26,400 25,420 26,400 26,430 1.14 1.13 2.54 30,700 30,600 30,950 30,800 30,950 30,800 0.81 0.65 1.906 32,350 32,000 32,600 33,150 32,600 32,150 0.77 0.47 1.27 35,300 35,000 35,650 35,000 35,650 35,000 0.98 0.00 0.63 40,20 40,700 40,600 40,700 40,600 40,300 1.22 0.74



						41
Volts/cm.						
50,000						
40,000	9					
30,000				xpermental		
			•	Peek Peek		-0-
20,000						
10,000						
0		2		7		
	0.	on of Sphe	res -		TE XIL	
				1968 2 66 2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	RISON OF	
				POTENTIAL	بالتراوي والبدائر ومناوع أوارت ويروو	
				L.M. Apga	- May 19,1	9/3



The Effect Of Foreign Materials In Air Gap.

To study the effect of materials of various specific inductive capacity upon the corona and striking voltage, a grounded brass plate was suspended between the terminals. The curve for this is compared to that of the plain gap in Plate 13, using one inch balls in both cases.

The str ing voltage with the brass plate in gap is a trifle higher than that of the plain air gap up to the critical point at which point it jumps from 77,500 to 113,500 volts and then follows the curve shown. The corona line is higher than in the case of simple air gap and nearly parallel to it.

When a glass plate is substituted for the brass one, the corona line is lower but parallel to the one for plain air.

Use of these principles mi ht be made in insulating high tension lines since the striking voltage is materially increased by the grounded brass plate.



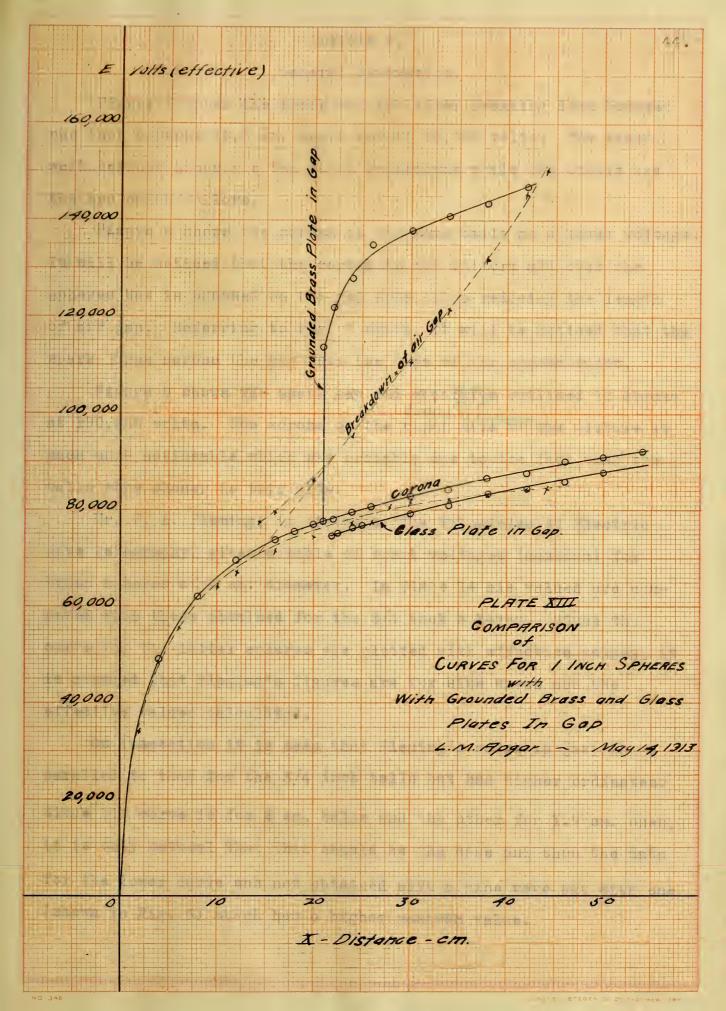
TABLE #11.

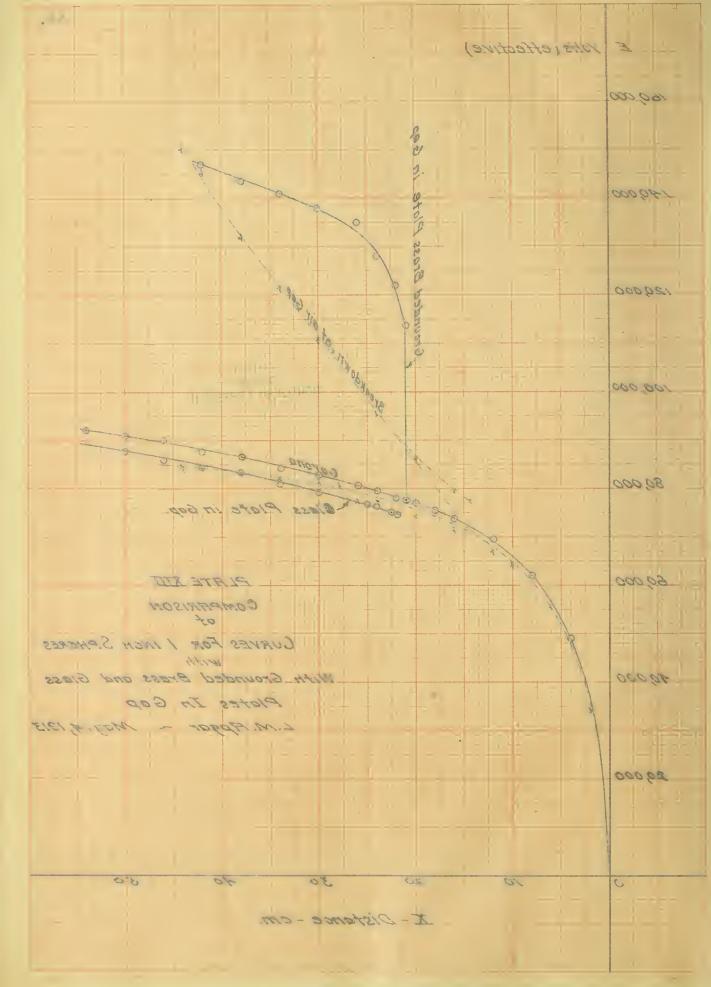
FO. 1 INCH S HELES.

GROUNDED BRASS PLATE IN GAP. GLASS PLATE IN G P.

x cm.	Corona Appears. KV.	Break-down.	Corona A-pears KV.
4 82 16 20 21 22 24 26 34 46 54	77.5 78.0 79.5 80.5 82.5 84.0 86.5 87.5 90.0 91.0	49.0 62.0 69.5 73.8 77.0 113.5 122.0 128.0 135.0 138.0 141.0 143.5 147.0	74.5 76.0 76.9 79.0 81.0 83.0 84.5 86.5 88.0







General Discussion.

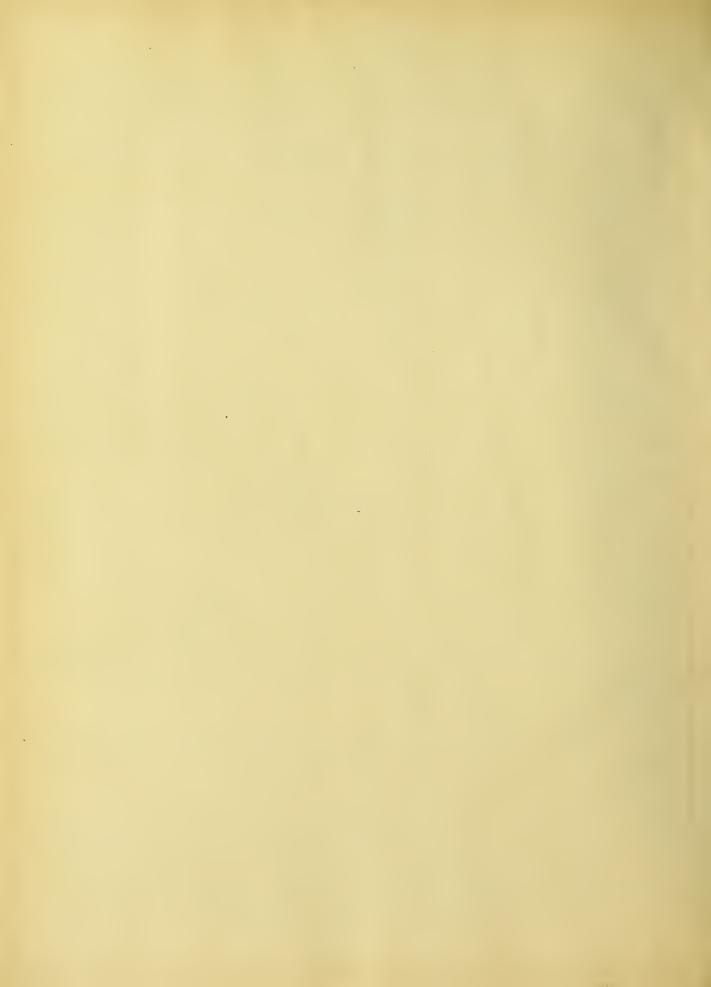
Figure 7 shows the spark and arc after breaking down between one inch spheres 18,5 cm. apart and at 83,000 volts. The sharp, well defined lines are the first breakdowns while the others are the arc which follows.

Figure 8 shows the corona on the same balls at a lower voltage. It will be noticed that the corona is not uniform all over the spheres but is bunched on the gap side, thus reducing the length of air gap. Referring to Fig. 7 again, it will be noticed that the spark jumps across the gap from the tips of the corona tufts.

Figure 9 shows the spark gap and apparatus outlined in corona at 190,000 volts. The corona on the right side of the picture is much more noticeable which was probably due to the fact that the walls were closer to this side.

Mr. J. A. Fleming, in his book "The Principles of Electric Wave Telegraphy," gives a table of spark voltages (maximum) for brass spheres of 2 cm. diameter. In Plate 14 his values are cmpared with those obtained for the 3/4 inch spheres. Since the curve for the latter spheres are plotted with effective values, it is assumed that Fleming's figures are for sine waves and the effective values calculated.

On inspection it is seen that Fleming's curve is just about paralled to that for the 3/4 inch balls but has higher ordinates. Since his curve is for 2 cm. balls and the other for 1.9 cm. ones, it is only natural that this should be the case and then the data for the lower curve was not obtained with a sine wave but with one (shown in Fig. 6) which has a higher maximum value.



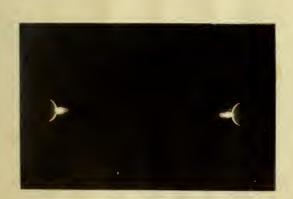
All the curves given by Pleming are of the same general shape as those given in the Plates but are only run for a few millimeters of spark gap; so that they are of no value for comparison at high voltages.

Peek in his paper "The Law Of Corona", gives the curves showing corona and breakdown for parallel conductors, which are of the
same general shape as those for spheres except that he does not
get the reverse curve in his spark line which was probably due to
the fact that he did not carry his voltage high en ugh.





F16. 7



F16.8



F16. 9



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V. CONCLUSION.

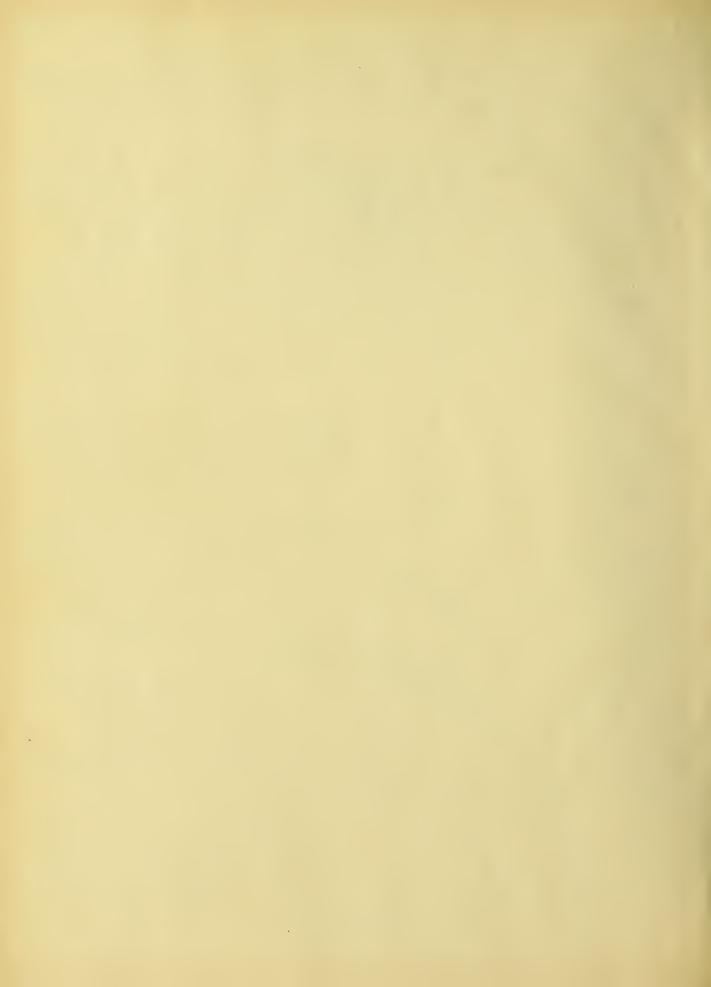
From observations during tests it was noted that a draft does not affect the voltage at which corona appears but it does raise the spark voltage.

The first appearance of corona is a very uncertain phenomena. Sometimes it is necessary to polish the spheres in order to obtain corona and then again it appears without. After this critical point is past both the corona and breakdown occur at the same respective voltages each time, that is, if the condition of the air is the same. After the air has broken down it will break again at a lower voltage if a draft is not used to remove the ionized air which acts as a conductor.

It was also proven that for spheres up to one inch in diameter that needles could be substituted at the critical point for the balls with the same results.

The theory that the potential gradient is a constant of the value 30,000 volts per cm. does not hold according to data obtained but the potential gradient depends upon the size of the spheres, varying in this case from 26,100 volts per cm. for 2 inch balls to 40,200 volts per cm. for 1/4 inch spheres.

If a grounded conductor is placed in the gap, the striking and corona voltages are increased. If a material of higher specific inductive capacity than air, like glass, is inserted in gap the corona voltage is lowered.



VI. REFERENCES.

The Principles Of Electric Wave Telegraphy.

by J. A. Fleming. Chaot. II.

Electricity and Magnetism.

by J.C. Maxwell. Vol. 1 Chapt. M.

A. I. E. E. Proceedings.

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